





DIRECT GEOREFERENCING OF STATIC TERRESTRIAL LASER SCANS

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For what purpose do we require 3D data?

- 3D city models for planning issues or documentation tasks, e.g., in architecture or forensics
- Typical tasks of geodetic engineering: deformation measurements or high-precise as-built documentation

What is an efficient and effective way of acquiring data?

- Rapid mapping using kinematic terrestrial laser scanning (k-TLS)
 - Mobile mapping: scanning of static objects from a moving platform
 - Fast scanning of static/kinematic objects from a static platform
- 3D data acquisition in an absolute or global coordinate system; required for several scenarios



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Motivation



Characteristics of k-TLS

- Fast high frequency and immediate 3D data acquisition
- High spatial resolution for short up to mid-ranges (<80m, phase-based laser scanner)
- Data acquisition in a relative or sensor-defined coordinate system

To-Do for using (k)-TLS data for above-named scenarios

- Observation of the laser scanner position and orientation
- Transform 3D data from local/sensor-defined to absolute/global coordinate system

Stockholm, 16.06.2008





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- State-of-the-art in georeferencing of static terrestrial laser scans
- Adapted sensor-driven method for direct georeferencing
 - Data acquisition and preprocessing
 - Robust estimation of the space curve
 - Projection of the 3D positions onto a best-fitting plane
 - Estimation of a best-fitting circle through the projected positions
 - Azimuth determination and result validation
 - Error budget
- Conclusions and future work



Terminology and brief overview of georeferencing

Registration Process of linking laser scans from different stations to one similar (local) coordinate system

Georeferencing Transformation of laser scans from a relative/local sensor system to an absolute/global coordinate sys.

- Indirect method: Georeferenced control points
- Direct method: Use of additional sensors
 Observation of the laser scanner position and orientation
- Data-driven method: Georeferenced data base

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System concept and aim of the presented method

- Use a minimized number of additional sensors
- Direct estimation of the laser scanner position and orientation
- Work without georeferenced control points
- Do not disturb the operation of the laser scanner
- Use to constant rotation of the laser scanner about the vertical axis as time and orientation reference
- High frequency data acquisition of a phase-based laser scanner demands a data-rate of at least 10 Hz for additional sensors



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Aim can be achieved by kinematic GNSS with a maximum number of 2 antennas to get the position and orientation



Data acquisition and preprocessing



- Place of measurements: "Ehrenhof" in the "Große Garten" of the "Herrenhäuser Gärten" in Hannover
- Data acquisition time approx. 15 minutes





Preprocessing: time synchronization

- 3D laser scan consists of several scan lines characterized by one turn of the vertical step motor
- Per scan line one ttl-impulse is available which is used for time synchronization task
- With the event marker input of the GNSS-receiver for every ttlimpulse a GPS timestamp is obtained and stored in the RINEX observation file
- Optional interpolation of missing ttl-impulses



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Unique time synchronization between scan lines and ttlimpulses is now given



Preprocessing: GNSS analysis

- Trajectory of the antenna reference point (ARP) described by the orbital motion of the laser scanner is a space curve
- 2 different approaches were performed to estimate the trajectory
 - (1) Calculation of a baseline between the local reference station and each antenna installed on top of the laser scanner
 - (2) Calculation of a relative baseline between the two antennas installed on top of the laser scanner

Software used for GNSS analysis: (1) *Trimble Total Control* by *Trimble*, (1) *Geonap* by Geo++ and (1) + (2) *Wa1* by *Lambert Wanninger*



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Calculation of an azimuth for each scan line in the 3D laser scan from the GPS trajectory

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Two step model of the robust parameter estimation

(1) Projection of the 3D positions onto a best-fitting plane

- Take in account the full 3D information of the points
- Consideration of rotations due to the coordinate transformations

(2) Estimation of a best-fitting circle through the projected positions

- Improvement of the azimuth determination by using adjusted/smoothed instead of original/noisy positions
- Robustness means here to perform Baarda's data-snooping for outlier detection and elimination
- Estimation is independent of the coordinate system
 - Here: transformation to the Gauss-Krüger System for comparison with terrestrial measurements by a tachymeter

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(1) Projection of 3D positions onto a best-fitting plane

- Orthogonal projection of 3D positions onto a best-fitting plane with a principal axis transformation (acc. to DRIXLER (1993))
 - Introducing centered point coordinates
 - Analysis of the perpendicular distances for all points
 - Comparison of all perpendicular distances in an iterative process according to the (1-α) quantile value of the normal distribution (α=1%)
 - Corresponding points to a rejected null hypothesis are eliminated
 - Perform normal projection of the centered points onto the plane
 - Perform principal axis transformation



Robust estimation of the space curve



data set /7001hg4lgn.bgk with GNSS analysis by wa1 and coordinate transformation by gn



Robust estimation of the space curve



data set /hg4thg4lgnCA.bgk with GPS analysis by wa1 and coordinate transformation by gn



(2) Estimation of a best-fitting circle through projected pos

- Use of known data-snooping method in circle adjustment by transferring the Gauss-Helmert model (GHM) into an equivalent Gauss-Markov model (GMM) (acc. to JÄGER ET AL. (2005))
- Instead of the plane adjustment (1) here in step (2) the stochastic information for the positions are considered
 - By a variance-covariance matrix given by the GNSS analysis the results for the circle adjustment could be improved
- In the end the adjusted positions as well as the center point are transformed to the original coordinate system (x-y-z) by the inverse principal component transformation



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Robust estimation of the space curve

(2) Estimation of a best-fitting circle through projected pos raw data and adjustment results in raw data and adjustment results in 3d centered raw data and 3d equal axis scaling adjustment results in 2d (u-v-plane) ocal reference station – *Leica* antenna 0.3 0.2 794.97 795.2 0.1 794.965 X [m] ^ z [m] 795 E "Absolute" baseline 794.96 -0.1 794.8 5.806965 5.806965 794.955 -0.2 3.5475 3.5475 3.5475 794.95 5.8065 y [m] -0.3 3.5475 5.8065 × 10 x [m] 3.5475 -0.2 0.2 0 3.5475 5.8065 x [m] u [m] 3.5475 y [m] 106 centered raw data in 2d (u-v-plane) (7711) raw data in 3d (7711) x 10 raw data in 3d (7711) adjusted data in 3d centered adjusted data in 2d (x-y-plane) adjusted data in 3d adjusted center point adjusted center point adjusted center point radius variation for estimated point positions range of variation in adjusted radius [m] 00 80 80 80 radius variation for adjusted point positions (7711) adjusted radius (0.304m) 0 1000 2000 3000 4000 5000 6000 7000 # positions

data set /7001hg4lgn.bgk with GNSS analysis by wa1 and coordinate transformation by gn



Robust estimation of the space curve

(2) Estimation of a best-fitting circle through projected pos



data set /hg4thg4lgnCA.bgk with GPS analysis by wa1 and coordinate transformation by gn



Azimuth determination

Azimuth Calculation for each scan line from GPS trajectory

- Δ azimuth between each scan line and the corresponding part of the GNSS trajectory
- Δ azimuth can be derived by the constant rotation of the laser scanner about its vertical axis



- Δ azimuth is constant if it is not affected by any faults
- Consideration of Δ azimuth at each vertical motor position of the laser scanner



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→ 3D laser scan referenced to a global coordinate system and/or start values for iterative algorithms for registration tasks

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Result validation

Tachymeter versus TLS directions



data set /hg4thg4lgnCA.bgk with GPS analysis by wa1 and coordinate transformation by gn



Separate inspection of hybrid sensor system components

Concentration only on that kind of errors which are directly concerning the presented approach

Laser scanner

- Trunnion axis error caused by the weight of the antennas
- Anomaly in the horizontal as well as vertical rotation speed GNSS component as well as GNSS analysis
- Near-field effects caused by the antenna adaption made of aluminum on the laser scanner or possibly multipath
- Alternating antenna orientation



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Adapted sensor-driven method for direct georeferencing

- Use of the constant rotation of the laser scanner in combination with kinematic GNSS for a direct observation of the laser scanner position and orientation
- Improved azimuth determination by a two step model for robust estimation of the space curve of the ARP
- Metric uncertainty of about 1 cm for the azimuth calculation on a distance up to 30 m



- Modify the antenna installation for the use with the Z+F IMAGER 5006
- Detailed investigations on the presented error budget
- Consider stochastic information for the plane adjustment
- Implementation of a robust parameter estimation

Acknowledgements

The authors thank Dipl.-Ing. Frank Hinsche from *Leica Geosystems* who has provided two *Leica GPS1200GX Pro* equipments. Also thanks are given to Vincent Meiser for the support during the data acquisition and very warmly thanks to Prof. Dr.-Ing. Lambert Wanninger for the GNSS analysis!

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